Acoustic Characterization of Two Megasonic Devices for Photomask Cleaning

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Wet photomask cleaning relies on megasonic agitation to enhance the process, but there are many challenges to reliably control performance in terms of particle removal efficiency (PRE) and damage. Typically all that is specified about the acoustic output is the driving frequency and the electric power delivered to a transducer. Although there are several studies on particle removal and pattern damage at 1 MHz, there is very little known about the cavitation performance at higher frequencies such as 2-4 MHz. Two transducer configurations are acoustically evaluated here to better understand how the acoustic waves interact with the substrate which is the basis to optimizing cleaning performance.



RESULTS & DISCUSSION

METHODS



Hydrophone in a Free Field 0.5 0.2 0.1 ν γ γ γ γ γ γ γ γ (mm) γ γ (mm) <u>χ(mm)</u> Μάμνημοτοκα 0.065 0.065 0.06 0.06 0.055 0.05 **Mask Sensor** 0.045 in a Standing 0.04 ഗ 0.035 0.03 > Wave Field 0.035 0.03 0.025 0.025 0.02 0.02 0.015 0.015 0.01 0.01 0.005 0.005 X (mm) δά 4 ώ ή - ο - ο ω 4 ω X (mm) 3 MHz Cone 1 MHz Cone Cone Hydrophone in a Free Field



Incident wave propagates at Incident wave disturbed by an off-angle from transducer; reflected wave from both top and bottom surface of quartz; standing waves pattern some waves transmit through consistent at 3 MHz the quartz mask

The resultant sound field reveal a complex pattern from multiple reflections; similar scaled pattern from both 1 and 3 MHz.











Nozzle & Cone: Varying Generator Power

CONCLUSIONS

Although the frequency and generator power settings are equivalent, the acoustic performance of the nozzle and cone transducers is significantly different. Clearly frequency and electrical power alone are not the only determinants of acoustic performance and the subsequent cleaning activity.

For the same input power, the direct field pressure output from the nozzle transducer is approximately 10 times greater than that from the cone transducer, certainly because of its smaller footprint. It is also observed that in both designs the pressure from cavitation is about two orders of magnitude lower than the direct pressures.

So, what physical mechanism from each megasonic transducer is





• Direct field pressure is \geq 10X higher than cavitation pressure for both nozzle and cone

• 3 MHz nozzle yields ~3X higher stable cavitation pressure than 3 MHz cone at generator powers of 1 and 2 W

• Low levels of transient cavitation pressure under all conditions

cleaning? The results presented here indicate a significantly higher level of direct field pressure than stable and transient cavitation pressure. However, the test conditions may not fully represent actual cleaning processes leaving this still an open question.

Schlieren imaging highlights the complex behavior of the sound waves propagating between the mask, transducer, and water surface. For instance, it shows the nozzle transducer jet angle affects the interference pattern. Imaging the cone transducer indicates that the incident wave propagates at an offset angle from transducer. The resultant sound field reveals a complex pattern from multiple reflections, yielding a "scrubbing" mechanism at both 1 and 3 MHz.

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